CO₂ power cycle development – tools and applications

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EFFORT KMB

Energy Efficiency in Offshore Oil and Gas Production





Goal: Reduced energy use and CO₂ emissions
Offshore specific: low weight and volume important
Funded: RCN 65%, Industry 35%

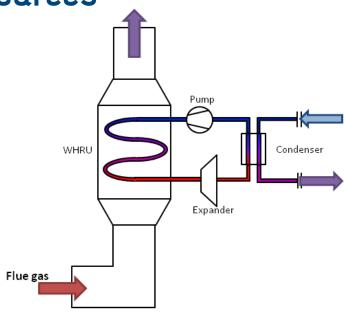
Kristin platform - Photo Marit Hommedal - Statoil



EFFORT project example:

Power Production from Surplus

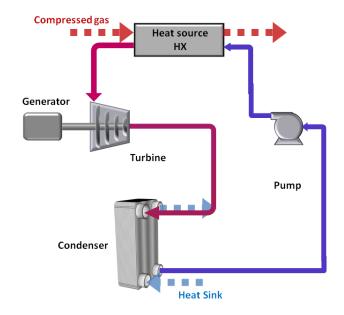
Heat Sources



High temperature gas turbine exhaust gas (550°C)

- Compact bottoming Rankine Cycles
 - Transcritical CO₂
 - Steam, once though boilers
 - Hydrocarbons



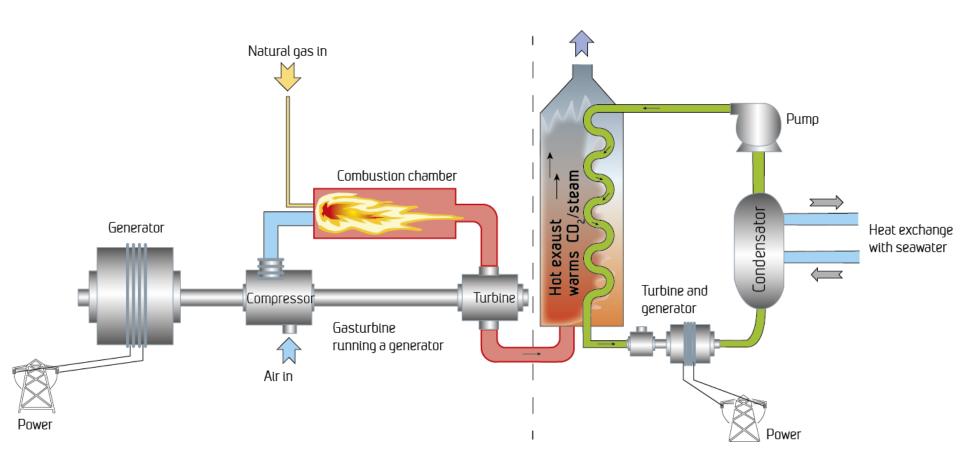


Low temperature compressed gas (150'C)

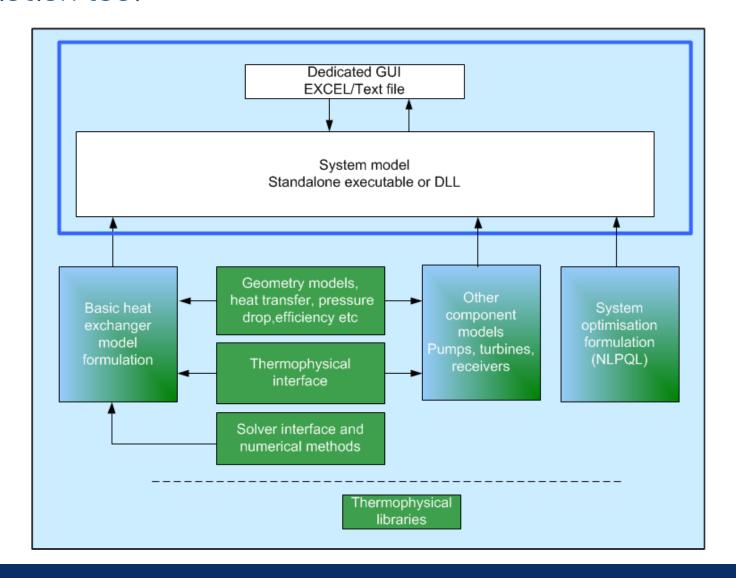
- High pressure -> compact HX
- Rankine Cycle
 - Subcritical hydrocarbon
 - Transcritical CO₂ or hydrocarbon



Application 2: CO₂ bottoming cycle for a Gas Turbine (GT)



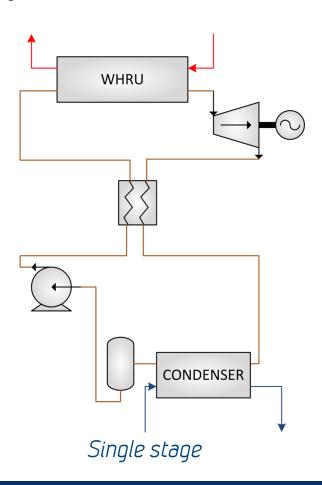
Simulation tool

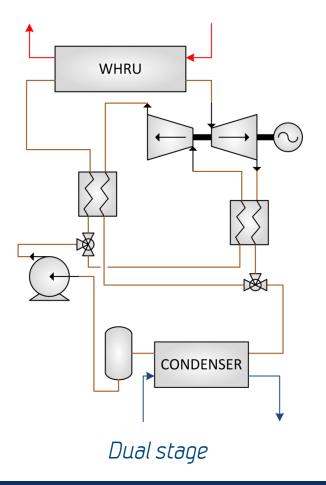




Off – design simulations

Two layouts are chosen based on HYSYS evaluation and inspiration from patents

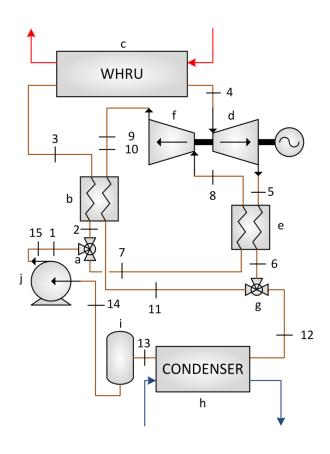






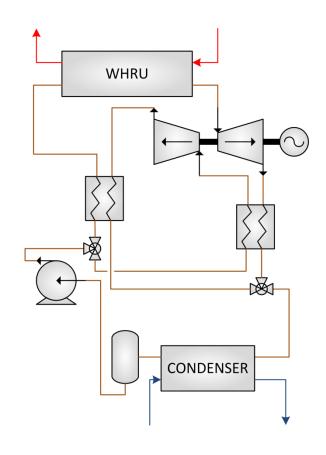
Model description

- FLEXHX heat exchangers
 - Tube and fin WHRU
 - Compact heat exchanger recuperators
 - Plate / plate and shell condenser
- Isentropic efficiency based turbomachinery
 - Improved models to be included when available
- Low pressure receiver
 - Balances the system and stabilizes integration
- NLPQL constrained optimization problem solver
 - System constrained variables
 - "Free" optimization variables



Boundary conditions, assumptions and design considerations

Ambient			
Temperature [°C]	15		
Pressure [bar]	1.013		
Relative humidity [%]	60		
Cooling water temperature [°C]	10		
Gas Turbine			
Model type	GE LM2500+G4 DLE		
Fuel	Methane		
Inlet pressure drop [bar]	0.010		
Bottoming Cycle			
WHRU UA* [kW/K]	400		
Recuperator 1 UA* [kW/K]	1000		
Recuperator 2 UA* [kW/K]	250		
Max pump outlet pressure [bar]	200		
Condensation temperature *[°C]	20		
Cooling water temperature increase [K]	10		
Pump efficiency [%]	80		
Expander efficiency [%]	85		
Motor/generator efficiency [%]	95		





^{*}Only at design, and will change at off-design

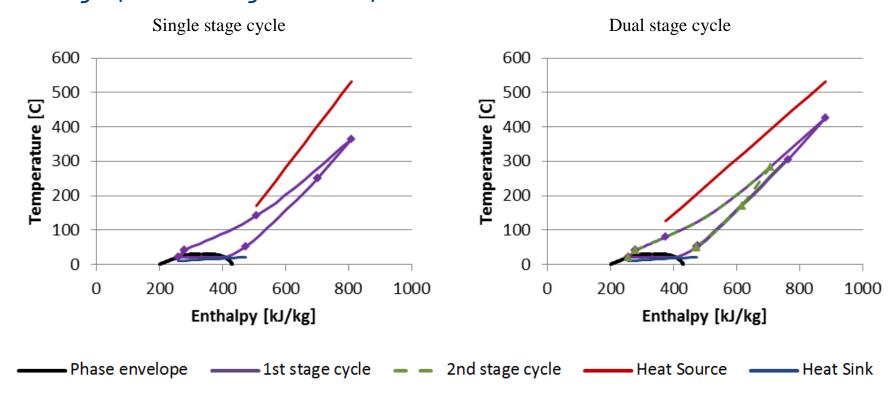
Design point - Main results

Plan type	Simple cycle	Combined cycle	Combined cycle
		single stage	dual stage
Gas Turbine	GE LM2500+G4	GE LM2500+G4	GE LM2500+G4
Net plant power output [MWe]	32.2	41.1	42.0
GT gross power output [MWe]	32.5	32.1	32.1
CO ₂ turbine shaft power [MW]	1	13.0	14.2
CO ₂ pump shaft power [MW]	1	2.7	2.9
CO ₂ BC gross power output [MWe]	-	9.5	10.4
Plant efficiency [%]	38.6	48.9	50.0
Exhaust mass flow [kg/s]	89.9	89.9	89.9
Exhaust Temperature after WHRU [°C]	528	170	126

- 28-30 % increase in net power output
- 10-11.5 %-points increase in total efficiency
- About 1 MWe difference between single and dual stage



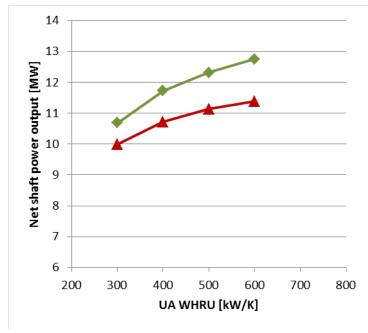
Design point - Cycle comparison

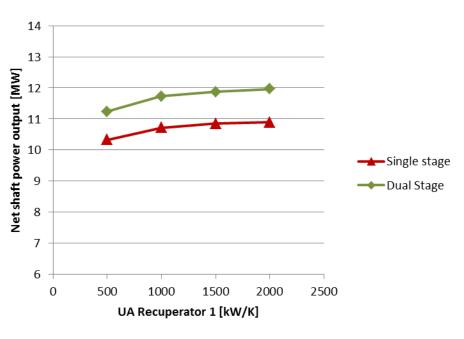




Design point - Cycle comparison

- The difference between the cycles will increase with increased WHRU size
 - Comparison performed with perfect counterflow heat exchangers



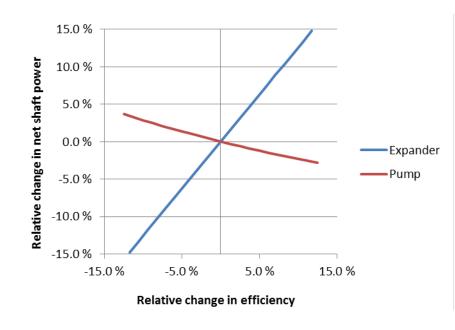


HYSYS evaluation of effect of heat exchanger size



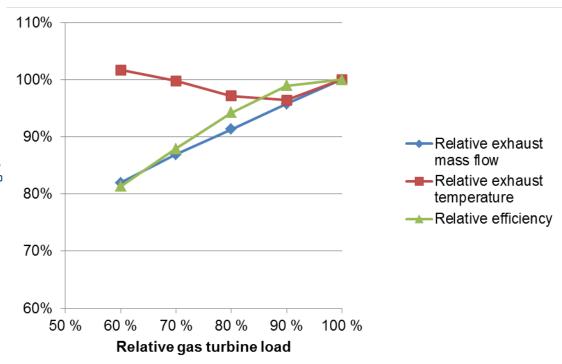
Influence of CO₂ turbomachinery efficiency

- Very limited information on CO₂ turbomachinery
 - Core technology for vendors
- High power density makes different challenges compared to conventional expanders
- Compared to steam, the pump efficiency important
- 5 % change in pump efficiency yields 1.3 % change in net shaft power output
- 5 % change in expander efficiency yields 6.3 % change in net shaft power output



Off-design - Gas turbine

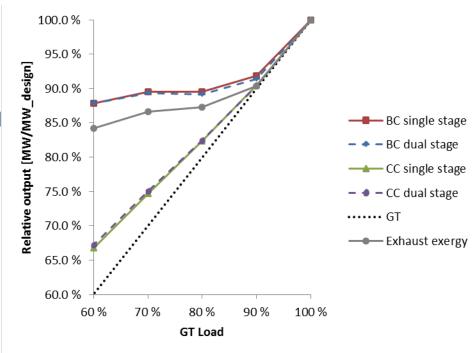
- Linear reduction in exhaust flow rate
- Increased exhaust temperature below 90 % load
 - Due to DLE fuel staging
- Rapid drop in efficiency below 90 % load





Off-design - Bottoming cycle

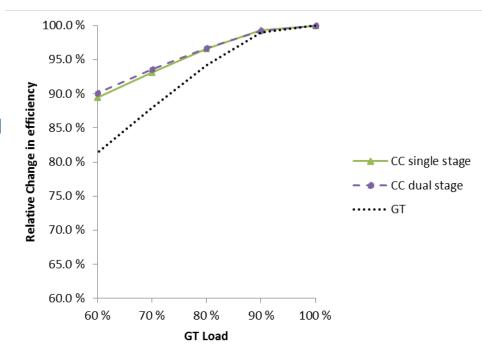
- Similar relative performance of the two cycles
- Increased exergy efficiency
 - Increased heat exchanger efficiency
 - Reduced pressure drop due to reduced flow rates
- Flattens total performance curves





Off-design - Bottoming cycle

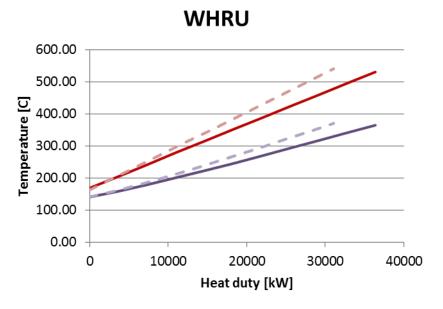
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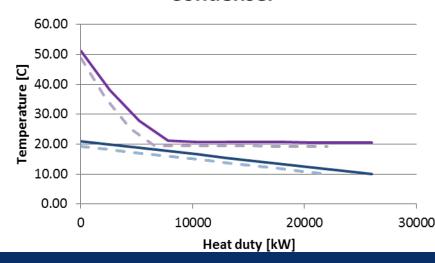


Off-design - Heat exchangers

- 100 % vs 60 % GT load
- WHRU and recuperator
 - $Q = UA\overline{\Delta T}$
 - Area is constant
 - Reduced flow rate → reduced heat transfer coefficient (U) and duty (Q)
 - Temperature difference ≈ constant
- Condenser
 - Water flow is constant
 - Reduced temperature difference
 - Reduced condensation pressure



Condenser





Summary Application: CO₂ bottoming cycle offshore

- Inclusion of **bottoming cycles** to gas turbines on offshore oil and gas installations could be an attractive solution for **improved energy efficiency and reduced emissions**. The results show that utilisation of $\mathbf{CO_2}$ as working fluid in the bottoming cycles could be a **viable alternative to steam**.
- The results show 8 and 16 % lower power output respectively for a dual- and single stage CO₂ cycle compared to compact steam bottoming cycles reported in literature. Taking into account the probable positive characteristics with respect to volume, weight, cost, which are important advantages especially for off-shore applications, the results are highly interesting.
- It is further shown that the **output can be increased if the heat exchanger sizes are increased or the efficiency of the turbomachinery is improved**. However, only a techno-economical optimisation may show if this is desirable.
- A further aspect is the advantageous off-design characteristics with the proposed control strategy. Gas turbine part load condition of 60% still maintains about 85% net power output from the CO₂ bottoming cycle, resulting in 67 % net plant output. Also the efficiency is kept higher at lower load, with 45 % net plant efficiency at 60 % GT load, compared to 31 % for only the gas turbine.
- The CO₂ bottoming cycle technology is not fully commercially available yet, and compared to steam cycles much less mature. Important development is however on-going and the technology is already demonstrated at scale, and full scale pilots are planned. This will give important information in verifying the results achieved through modelling and simulation.



Thank you for your attention!

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